



COMPUTATIONAL SCHEME FOR GEOSYNCHRONOUS SATELLITE ORBIT DUE TO GRAVITATIONAL ANOMALY OF THE EARTH

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ABSTRACT

By analysing the influence of the earth's gravitational anomaly on the orbit of a satellite around the earth, a computational scheme for geosynchronous satellite orbit with small inclination is developed. The governing equations of motion, which consist of three equations and have been simplified to take into account geosynchronous conditions and small displacements, are solved by numerical technique. In particular the radius of geosynchronous orbit is obtained by solving the first governing equation by Regula-Falsi method. Stationary points are obtained by indirect method, i.e. by first finding the longitude positions with zero longitudinal accelerations. The trajectory of the subsatellite point is obtained by solving the governing equations for small displacements by Runge-Kutta method. Comparison of computational result with Blitzer's and Flury's, using IAU 1968 and GEM-8 data, leads confidence to the present scheme.

I. INTRODUCTION

In an effort to develop satellite orbital computational program for satellite design studies, a computation scheme will be set up to calculate geostationary satellite orbits. The orbit of geostationary satellite will be influenced by earth's gravitational field, the gravitational field of the moon and the sun, and solar radiation pressure.

The earth's gravitational anomaly, the gravitational fields of moon and the sun, and solar radiation pressure will give rise to perturbation forces that perturb the orbit from its general elliptic shape. Specifically, the satellite orbit will not be truly geostationary, and the satellite will experience some drift.

In the present work, only the earth's gravitational anomaly will be taken into account, while perturbation due to the gravitational fields of the moon and the sun and solar radiation pressure will be dealt with in the future. The earth's gravitational potential will be represented as spherical harmonics ⁽¹⁾ ⁽²⁾ ⁽³⁾.

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The computational scheme outlined is a straight forward one. Several earth models will be utilized, and the accuracy of the computational program will be investigated.

II. GOVERNING EQUATIONS

Since the geostationary satellite considered is moving in the same direction as the direction of earth's rotation, it will be of great advantage to utilize a frame of reference rotating with the earth. It is then decided to use geocentric coordinate system which rotates with an angular speed ω_e which has the same magnitude and direction as the earth's rotational speed, as shown in Figure 1.

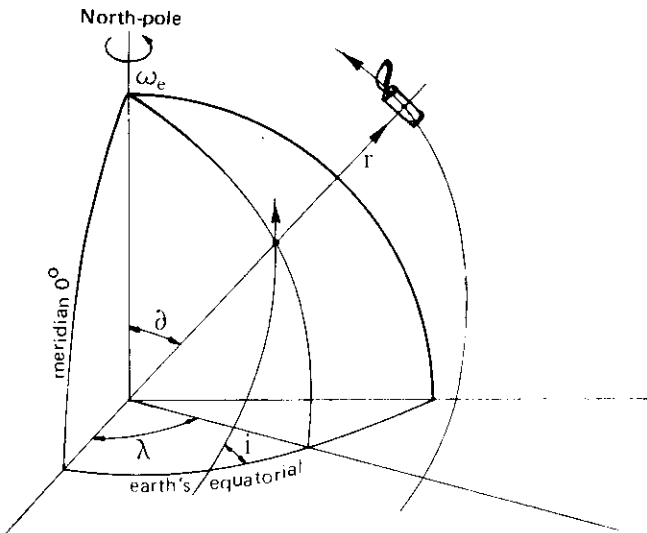


Figure 1 Coordinate System

For origin located at the center of mass of the earth, the gravitational potential can be expressed by ^{(1) (2) (3)}

$$V = - \frac{\mu}{r} \left[1 + \sum_{n=2}^{\infty} \sum_{m=0}^n \left(\frac{R}{r} \right)^n P_{nm} (\cos \theta) \right. \\ \left. \cdot (C_{nm} \cos m \lambda + S_{nm} \sin m \lambda) \right] \tag{1}$$

where :

- r geocentric radius
- R earth's equatorial radius
- θ colatitude
- μ product of the gravitational constant and the mass of the earth ($=kM$)

P_{nm} - associated Legendre polynomials

C_{nm}, S_{nm} - satellite coefficients (tesseral harmonic coefficients)

and :

$$P_n(x) = \frac{1}{2^n n!} \frac{d^n}{dx^n} (x^2 - 1)^n ; P_{nm}(x) = (1 - x^2)^{m/2} \frac{d^m P_n(x)}{dx^m}$$

Now letting :

$$J_n = -C_{n0}, \text{ the zonal harmonic coefficients}$$

$$J_{nm} = (C_{nm}^2 + S_{nm}^2)^{1/2}$$

$$\lambda_{nm} = \frac{1}{m} \tan^{-1} (S_{nm}/C_{nm})$$

the tesseral harmonic coefficients can be eliminated from equation (1) which is then recast into the following form :

$$V = -\frac{\mu}{r} \left[1 - \sum_{n=2}^{\infty} J_n \left(\frac{R}{r}\right)^n P_n(\cos \theta) + \sum_{n=2}^{\infty} \sum_{m=1}^n J_{nm} \left(\frac{R}{r}\right)^n P_{nm}(\cos \theta) \cos m(\lambda - \lambda_{nm}) \right] \quad (2)$$

The kinetic energy per unit mass of satellite in an orbit around the earth can be represented by:

$$E_k = 1/2 [\dot{r}^2 + r^2 \dot{\theta}^2 + r^2 \sin^2 \theta (\dot{\lambda} + \omega_e)^2] \quad (3)$$

The corresponding total energy per unit mass can generally be represented by:

$$E = E_k - V \quad (4)$$

where V is the potential energy per unit mass which is equivalent to the earth's gravitational potential at the satellite center of mass.

The equation of motion of the satellite can then be derived by utilizing Lagrange equation⁽⁴⁾, i.e. :

$$\frac{d}{dt} \left(\frac{\partial E}{\partial \dot{r}} \right) - \frac{\partial E}{\partial r} = 0$$

$$\frac{d}{dt} \left(\frac{\partial E}{\partial \dot{\lambda}} \right) - \frac{\partial E}{\partial \lambda} = 0 \quad (5)$$

$$\frac{d}{dt} \left(\frac{\partial E}{\partial \dot{\theta}} \right) - \frac{\partial E}{\partial \theta} = 0$$

where r, λ dan θ are spherical coordinates commonly utilized.

Substituting equation (3) in equation (4) and taking its derivatives in spherical coordinates and their time derivatives, one obtains :

$$\frac{\partial E}{\partial r} = r \dot{\theta}^2 + r (\dot{\lambda} + \omega_e)^2 \sin^2 \theta - \frac{\partial V}{\partial r}$$

$$\frac{\partial E}{\partial \dot{r}} = \dot{r}$$

$$\frac{\partial E}{\partial \dot{\lambda}} = - \frac{\partial v}{\partial \lambda} \quad (6)$$

$$\frac{\partial E}{\partial \dot{\lambda}} = r^2 (\dot{\lambda} + \omega_e) \sin^2 \theta$$

$$\frac{\partial E}{\partial \dot{\theta}} = r^2 (\dot{\lambda} + \omega_e)^2 \sin \theta \cos \theta - \frac{\partial v}{\partial \theta}$$

$$\frac{\partial E}{\partial \dot{\theta}} = r^2 \dot{\theta}$$

Substitution of equation (6) into equation (5) yields :

$$\ddot{r} - r \dot{\theta}^2 - r (\dot{\lambda} + \omega_e)^2 \sin^2 \theta + \frac{\partial v}{\partial r} = 0 \quad (7)$$

$$\frac{d}{dt} [r^2 (\dot{\lambda} + \omega_e) \sin^2 \theta] + \frac{\partial v}{\partial \lambda} = 0 \quad (8)$$

$$\frac{d}{dt} (r^2 \dot{\theta}) - r^2 (\dot{\lambda} + \omega_e)^2 \sin \theta \cos \theta + \frac{\partial v}{\partial \theta} = 0 \quad (9)$$

To obtain a general solution, it is convenient to recast equations (7) to (9) into nondimensional form by defining the following dimensionless parameters:

$$Z = \frac{r}{R}$$

$$\tau = \omega_e t \quad (10)$$

$$\alpha = \frac{\mu}{\omega_e^2 R^3}$$

We then obtain :

$$\begin{aligned} \ddot{z} - z \dot{\theta}^2 - (1 + \dot{\lambda})^2 z \sin^2 \theta + \frac{\alpha}{z^2} \left[1 - \sum_n \frac{(n+1)J_n}{z^n} P_n(\cos \theta) \right. \\ \left. + \sum_n \sum_m \frac{(n+1)J_{nm}}{z^n} P_{nm}(\cos \theta) \cos m(\lambda - \lambda_{nm}) \right] = 0 \end{aligned} \quad (11)$$

$$\begin{aligned} \frac{d}{d\tau} \left[(1 + \dot{\lambda}) z^2 \sin^2 \theta \right] + \alpha \sum_n \sum_m \frac{m J_{nm}}{z^{n+1}} P_{nm}(\cos \theta) \\ \cdot \sin m(\lambda - \lambda_{nm}) = 0 \end{aligned} \quad (12)$$

$$\begin{aligned} \frac{d}{d\tau} \left(z^2 \dot{\theta} \right) - (1 - \dot{\lambda})^2 z^2 \sin \theta \cos \theta - \alpha \sum_n \frac{J_n}{z^{n+1}} \sin \theta P'_n(\cos \theta) \\ + \alpha \sum_n \sum_m \frac{J_{nm}}{z^{n+1}} \sin \theta P'_{nm}(\cos \theta) \cos m(\lambda - \lambda_{nm}) = 0 \end{aligned} \quad (13)$$

where the dotted variables indicate their derivatives with respect to dimensionless time τ . These are the governing equations of motion of the satellite.

III. RADIUS OF SYNCHRONOUS ORBIT

The radius of synchronous orbit is the distance between the satellite and center of mass of the earth at which the radial acceleration due to kinetic (angular motion) and potential (gravitational potential) energy is zero. Since in addition a true geosynchronous orbit lies in the equatorial plane ($\theta = 90^\circ$), then equation (11) reduced to :

$$\begin{aligned} z - \left(\frac{\alpha}{z^2} \right) \left[1 - \sum_{\substack{n \\ \text{even}}} \frac{(n+1)J_n A_n}{z^n} \right. \\ \left. + \sum_{\substack{n-m \\ \text{even}}} \sum \frac{(n+1)J_{nm} A_{nm}}{z^n} \cos m(\lambda - \lambda_{nm}) \right] = 0 \end{aligned} \quad (14)$$

where even subscript signifies even values: in equation (14), we have taken advantage of the fact that for $\theta = 90^\circ$,

$$\begin{aligned}
 P_n(\cos \theta) &= A_n = \frac{(-1)^{n/2} n!}{2^n \left(\frac{n}{2}\right)! \left(\frac{n}{2}\right)!} && \text{for } n \text{ even} \\
 P_{nm}(\cos \theta) &= A_{nm} = \frac{(-1)^{(n-m)/2} (n+m)!}{2^n \left(\frac{n-m}{2}\right)! \left(\frac{n+m}{2}\right)!} && \text{for } (n-m) \text{ even} \quad (15) \\
 P_n(\cos \theta) &= P_{nm}(\cos \theta) = 0 && \text{for } n \text{ and } (n-m) \text{ odd}
 \end{aligned}$$

Equation (14) can be solved by numerical approach to give the values of the radius of synchronous orbits Z for any value of longitude λ .

Longitudinal Acceleration

At any longitudinal position, the longitudinal acceleration of the satellite can be calculated from equation (12), which can be rewritten into :

$$\ddot{\lambda} = - \frac{\alpha}{z^2 \sin^2 \theta} \sum_n \sum_m \frac{m J_{nm}}{z^{n+1}} P_{nm}(\cos \theta) \sin m(\lambda - \lambda_{nm}) \quad (16)$$

or, noting that $\theta = 90^\circ$:

$$\ddot{\lambda} = - \alpha \sum_{\substack{(n-m) \\ \text{even}}} \sum \frac{m J_{nm} A_{nm}}{z^{n+3}} \sin m(\lambda - \lambda_{nm}) \quad (17)$$

Using the value of Z obtained from equation (14), then equation (17) can be readily evaluated.

IV. STATIONARY CONDITIONS

Equation (11), (12) and (13) contain stationary conditions, at which the satellite experiences no radial acceleration, and its angular velocity exactly equals to the angular velocity of the earth. Such condition is represented by sets of values of Z , θ and λ which are constant, i.e. :

$$\begin{aligned}
 z &= z_0 = \text{constant} \\
 \lambda &= \lambda_0 = \text{constant} \\
 \theta &= \theta_0 = \frac{\pi}{2} - \delta_0 = \text{constant}
 \end{aligned}
 \tag{18}$$

where δ is the geocentric latitude, which is not zero, although small. In the geocentric frame of reference which rotates with the earth, then $\ddot{Z}, \dot{Z}, \ddot{\lambda}, \dot{\lambda}, \ddot{\theta}$ and $\dot{\theta}$ are equal zero, thus reducing equations (11), (12) and (13) to:

$$\begin{aligned}
 z_0 \cos^2 \delta_0 - \frac{\alpha}{z_0^2} \left[1 - \sum_n \frac{(n+1) J_n}{z_0^n} P_n(\sin \delta_0) + \sum_n \sum_m \frac{(n+1)}{z_0^n} \right. \\
 \left. \cdot J_{nm} P_{nm}(\sin \delta_0) \cos m(\lambda_0 - \lambda_{nm}) \right] = 0
 \end{aligned}
 \tag{19}$$

$$\sum_n \sum_m \frac{m J_{nm}}{z_0^n} P_{nm}(\sin \delta_0) \sin m(\lambda_0 - \lambda_{nm}) = 0
 \tag{20}$$

$$\begin{aligned}
 z_0^2 \sin \delta_0 + \alpha \sum_n \frac{J_n}{z_0^{n+1}} P'_n(\sin \delta_0) - \alpha \sum_n \sum_m \frac{J_{nm}}{z_0^{n+1}} P'_{nm}(\sin \delta_0) \\
 \cdot \cos m(\lambda_0 - \lambda_{nm}) = 0
 \end{aligned}
 \tag{21}$$

Since the shape of the earth is almost symmetrical and the value of J_{nm} is small, then δ_0 can be expected to be small. Hence the values of the Legendre and its associated polynomials in δ_0 can be approximated, following

Blitzer⁽⁵⁾, by :

$$\begin{aligned}
 P_n(\sin \delta_0) &= A_n \\
 P_{nm}(\sin \delta_0) &= A_{nm} \\
 P'_n(\sin \delta_0) &= D_n \delta_0 \\
 P'_{nm}(\sin \delta_0) &= D_{nm} \delta_0
 \end{aligned}
 \quad \text{for } n \text{ and } (n-m) \text{ even}$$

$$\begin{aligned}
 P_n(\sin \delta_0) &= B_n \delta_0 \\
 P_{nm}(\sin \delta_0) &= B_{nm} \delta_0 \\
 P'_n(\sin \delta_0) &= B_n \\
 P'_{nm}(\sin \delta_0) &= B_{nm}
 \end{aligned}
 \quad \text{for } n \text{ and } (n-m) \text{ odd}$$

(22)

where:

$$\begin{aligned}
 A_n &= \frac{(-1)^{n/2} n!}{2^n \left(\frac{n}{2}\right)! \left(\frac{n}{2}\right)!} \\
 A_{nm} &= \frac{(-1)^{(n-m)/2} (n+m)!}{2^n \left(\frac{n-m}{2}\right)! \left(\frac{n+m}{2}\right)!} \\
 B_n &= \frac{(-1)^{(n-1)/2} (n+1)!}{2^n \left(\frac{n-1}{2}\right)! \left(\frac{n+1}{2}\right)!} \\
 B_{nm} &= \frac{(-1)^{(n-m-1)/2} (n+m+1)!}{2^n \left(\frac{n-m-1}{2}\right)! \left(\frac{n+m+1}{2}\right)!} \\
 D_n &= \frac{(-1)^{(n+2)/2} (n+2)! (n^2+n)}{2^{n+1} \left(\frac{n}{2}\right)! \left(\frac{n+2}{2}\right)! (n+1)} \\
 D_{nm} &= \frac{(-1)^{(n-m+2)/2} (n+m+2)! (n^2-m^2+n)}{2^{n+1} \left(\frac{n-m}{2}\right)! \left(\frac{n+m+2}{2}\right)! (n+m+1)}
 \end{aligned}
 \quad (23)$$

Substituting these values in equations (19) to (21), one obtains :

$$z_0^3 - \alpha \left[1 - \sum_{\substack{n \\ \text{even}}} \frac{(n+1) J_n A_n}{z_0^n} + \sum_{\substack{n-m \\ \text{even}}} \sum \frac{(n+1) J_{nm} A_{nm}}{z_0^n} \cos m (\lambda_0 - \lambda_{nm}) \right] = 0 \quad (24)$$

$$\sum_{\substack{n-m \\ \text{even}}} \sum \frac{m J_{nm} A_{nm}}{z_0^n} \sin m (\lambda_0 - \lambda_{nm}) = 0 \quad (25)$$

$$z_0^3 \delta_0 + \alpha \sum_{\substack{n \\ \text{odd}}} \frac{J_n B_n}{z_0^n} - \alpha \sum_{\substack{n-m \\ \text{odd}}} \sum \frac{J_{nm} B_{nm}}{z_0^n} \cos m (\lambda_0 - \lambda_{nm}) = 0 \quad (26)$$

Equations (24), (25) and (26) can be solved numerically to obtain the sets of stationary values $(z_0, \lambda_0, \delta_0)$.

V. MOTION AROUND STATIONARY POINTS

In reality, the motion of geostationary satellite is not truly geostationary, but drifting around its geostationary positions. Such a condition can be represented by:

$$\begin{aligned} z &= z_0 + \Delta \\ \lambda &= \lambda_0 + \phi \\ \delta &= \delta_0 + \beta \end{aligned} \quad (27)$$

where $\Delta \ll 1$, $\phi \ll \pi$ and $\beta \ll \pi$

To obtain this motion, equation (26) is substituted into equations (24) (25)

and (26) and then linearizing by ignoring square and product terms in Δ , ϕ , β , and their derivatives, we find⁽⁵⁾ :

$$\ddot{\Delta} - (1+a)\Delta - 2z_0 \dot{\phi} + c\phi + e\beta = 0 \quad (28)$$

$$z_0^2 \ddot{\phi} + b\phi + 2z_0 \ddot{\Delta} + c\Delta + f\beta = 0 \quad (29)$$

$$\ddot{\beta} + (1+k)\beta + (e/z_0^2)\Delta + (f/z_0^2)\phi = 0 \quad (30)$$

where :

$$\begin{aligned}
 a &= \frac{2\alpha}{z_0^3} \left[1 - \sum_{\substack{n \\ (\text{even})}} \frac{(n+1)(n+2)J_n A_n}{2z_0^n} \right. \\
 &\quad \left. - \sum_{\substack{n-m \\ (\text{even})}} \frac{(n+1)(n+2)J_{nm} A_{nm}}{2z_0^n} \cos m(\lambda_0 - \lambda_{nm}) \right] \\
 b &= \alpha \sum_{\substack{n-m \\ (\text{even})}} \sum \frac{m^2 J_{nm} A_{nm}}{z_0^{n+1}} \cos m(\lambda_0 - \lambda_{nm}) \\
 c &= -\alpha \sum_{\substack{n-m \\ (\text{even})}} \sum \frac{m(n+1)J_{nm} A_{nm}}{z_0^{n+2}} \sin m(\lambda_0 - \lambda_{nm}) \\
 e &= -\alpha \sum_{\substack{n \\ (\text{odd})}} \frac{(n+1)J_n B_n}{z_0^{n+2}} + \alpha \sum_{\substack{n-m \\ (\text{odd})}} \sum \frac{(n+1)J_{nm} B_{nm}}{z_0^{n+2}} \\
 &\quad \cdot \cos m(\lambda_0 - \lambda_{nm}) \\
 f &= \alpha \sum_{\substack{n-m \\ (\text{odd})}} \sum \frac{m J_{nm} B_{nm}}{z_0^{n+1}} \sin m(\lambda_0 - \lambda_{nm}) \\
 k &= \alpha \sum_{\substack{n \\ (\text{even})}} \frac{J_n D_n}{z_0^{n+3}} - \alpha \sum_{\substack{n-m \\ (\text{even})}} \sum \frac{J_{nm} D_{nm}}{z_0^{n+3}} \cos m(\lambda_0 - \lambda_{nm})
 \end{aligned} \quad (31)$$

Equations (28) to (30) can be solved if the initial conditions Δ_0 , $\dot{\Delta}_0$, ϕ_0 , $\dot{\phi}_0$, β_0 and $\dot{\beta}_0$, are known, and hence the position, velocity and acceleration of the satellite during the course of its motion can be determined.

VI. DATA AND COMPUTATIONAL ASPECTS

Computational Scheme

Equation (14) can be solved for the radius of synchronous orbit Z by utilizing Regula Falsi method. Thus the values of Z for various longitudinal positions can be obtained and plotted. By substituting values of Z for any longitudinal positions in equation (16), one can obtain the longitudinal accelerations λ .

The positions of stationary points (z_0, λ_0, δ_0) can be obtained from equations (25) and (26) for λ_0 and δ_0 , respectively. To obtain z_0 values, an alternative method which is more expeditious than solving equation (24), and hence avoiding simultaneous solution of equations (24), (25) and (26) is utilized. For this purpose, z_0 values are solved by identifying longitudinal positions where the longitudinal acceleration vanishes and employ these values to obtain z_0 .

Next, simultaneous differential equations (28), (29) and (30) which represent the equations of motion of the satellite about its stationary points, are solved by utilizing Runge-Kutta method. For other points along the geosynchronous orbit the system of equations (11), (12) and (13) have to be solved instead of (28), (29) and (30) by using solutions of the latter system of equations as initial approximation. Direct solution of equations (11), (12) and (13) is presently being worked out.

Figure 2, 3 and 4 outline the algorithms used for the computational procedures mentioned above.

Earth and satellite coefficients data

Two sets of data are utilized in the computation; these are the earth and satellite coefficients data given by International Astronomical Union (IAU) in 1968, as tabulated in reference 6, reproduced in Table 1, and Goddard Earth Model 8 (GEM 8) published in reference 7, and reproduced in Table 2.

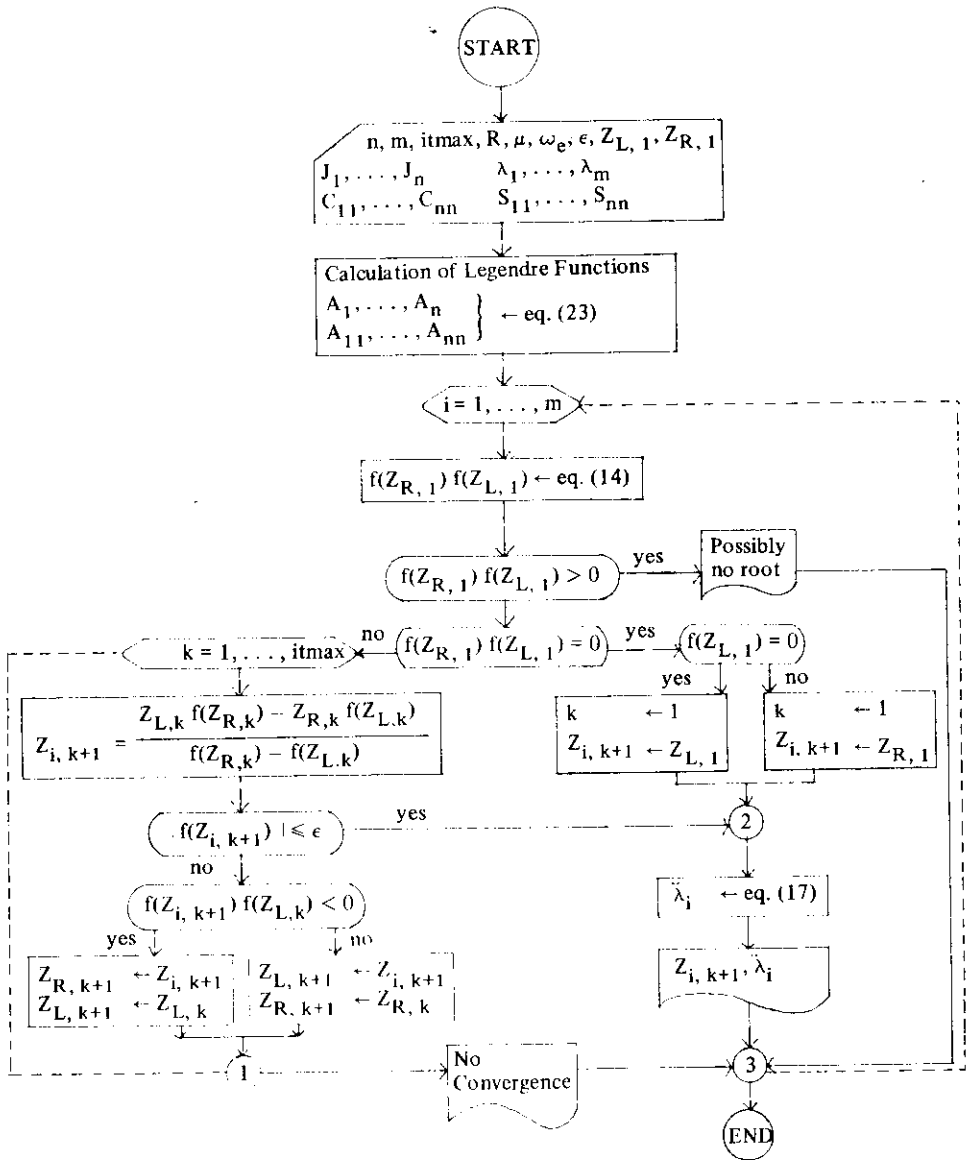


Figure 2 Flow chart for the solution of equation (14) with Regula-Falsi method.

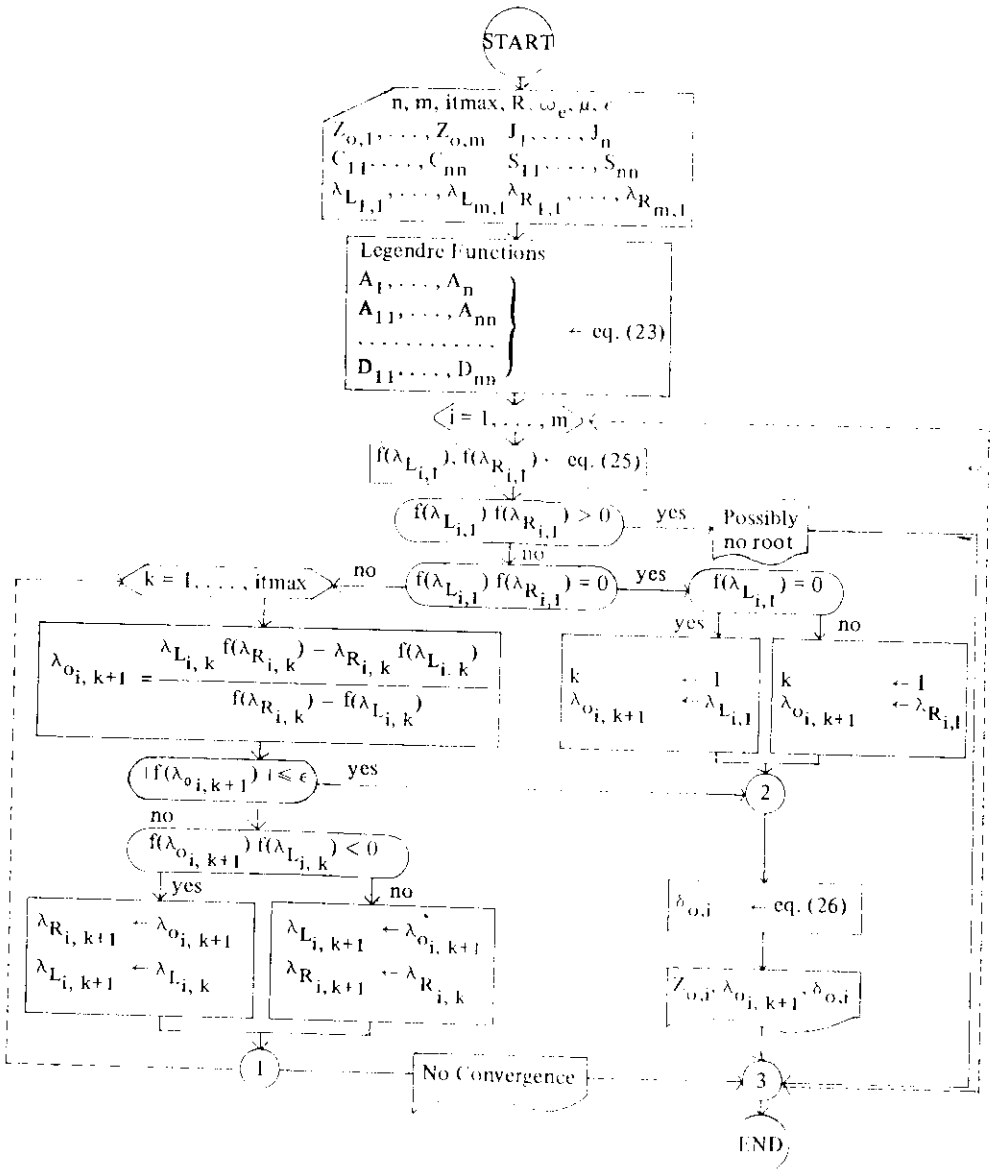


Figure 3 Flow chart for the solution of equation (25) using Regula-Falsi method

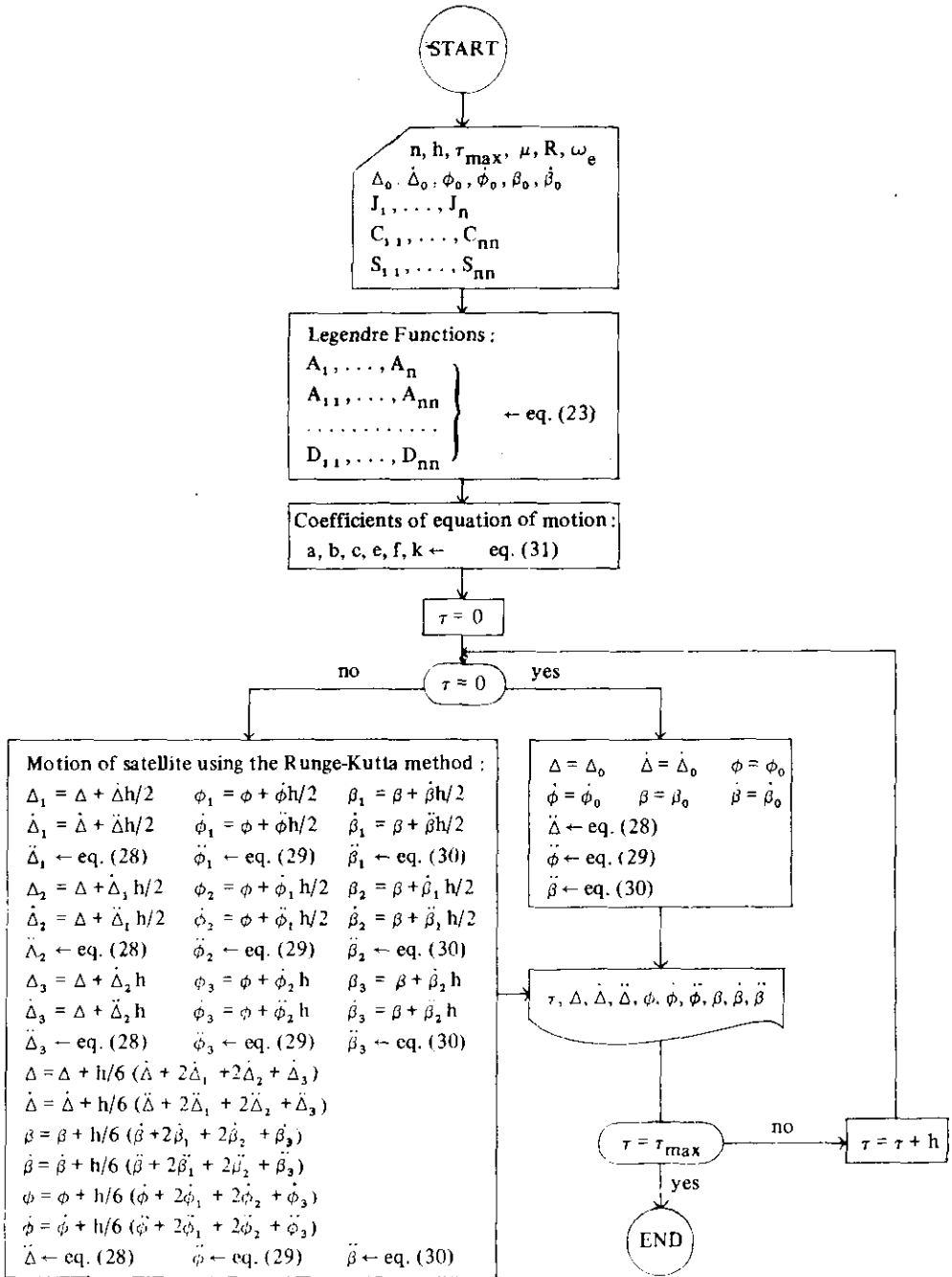


Figure 4 Flow chart for the solution of equation (28), (29) and (30) by using Runge-Kutta method

TABLE 1. Coefficients of the Geopotential for IAU 1968

$\mu = 3.986 \times 10^5 \text{ km}^3/\text{sec}^2$; $R = 6378 \text{ km}$

n	$10^6 J_n$	nm	$10^6 C_{nm}$	$10^6 S_{nm}$
2	1082.70	21	0.0000	0.0000
3	- 2.56	22	1.5700	- 0.8970
4	- 1.58	31	2.1000	0.1600
5	- 0.15	32	0.2500	- 0.2700
6	0.59	33	0.0770	0.1730
7	- 0.44	41	- 0.5800	- 0.4600
		42	0.0740	0.1600
		43	0.0530	0.0040
		44	- 0.0065	0.0023

TABLE 2. Coefficients of the Geopotential for GEM-8*

$\mu = 3.986008 \times 10^5 \text{ km}^3/\text{sec}^2$; $R = 6378.145 \text{ km}$

n	$10^6 J_n$	n m	$10^6 C_{nm}$	$10^6 S_{nm}$
2	1082.6254	2 1	- 0.0001	0.0004
3	- 2.5357	2 2	1.5710	- 0.9007
4	- 1.6200	3 1	2.1940	0.2696
5	- 0.2259	3 2	0.3066	- 0.2129
6	0.5426	3 3	0.0999	0.1976
7	- 0.3613	4 1	- 0.5098	- 0.4495
8	- 0.2066	4 2	0.0777	0.1489
9	- 0.1142	4 3	0.0589	- 0.0118
10	- 0.2475	4 4	- 0.0041	0.0065
..
29	- 0.0238	30 28	- 0.8558 $\times 10^{-40}$	0.1019 $\times 10^{-41}$

* Coefficients of the geopotential are derived from the normalized values given by GEM-8 (1977).

VII. DISCUSSION OF RESULTS

Taking into account the earth's gravitational anomaly, the radius of synchronous orbit $r = ZR$ is obtained by solving equation (16) and shown in Figure 5. The values of r varies from 42164, 7830 km to 42164.7952 km, where the smallest value occurs at $\lambda = 75^\circ$ and the largest value occurs at $\lambda = 162.5^\circ$.

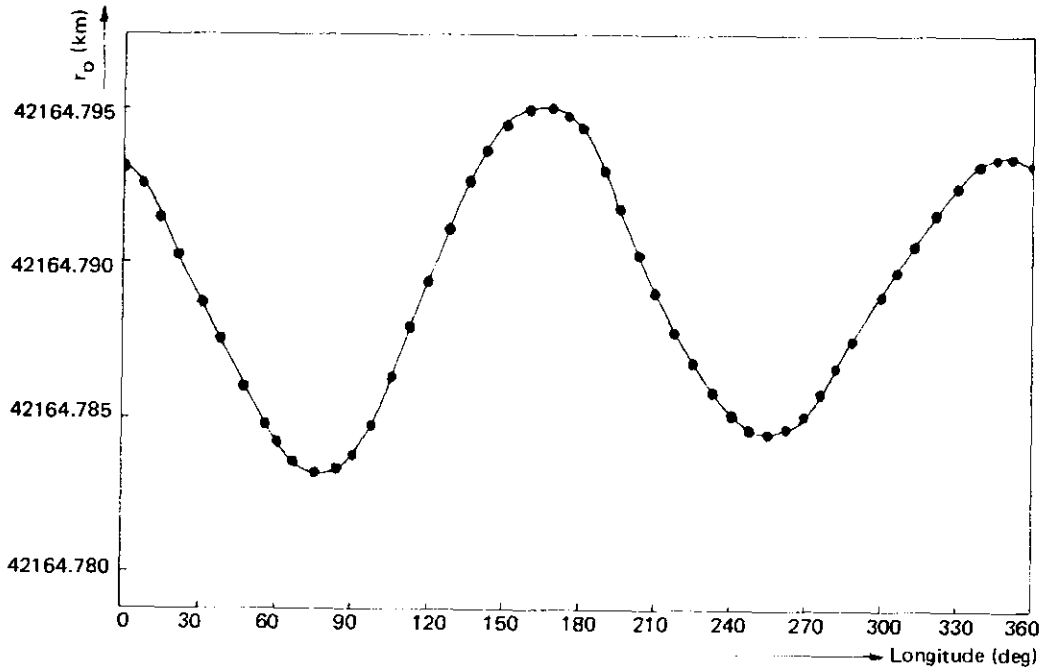


Figure 5 Radius of Synchronous Orbit

If the influence of the earth oblateness (J_2) alone is taken into account, the radius of geosynchronous orbit turns out to be 42164.78687 km for any longitude. This value can be compared with the radius of Keplerian orbit (without considering the gravitational anomaly) of 42164.26687 km. Thus the influence of J_2 is increasing the geosynchronous orbit by 520 m, while higher order terms of the gravitational anomaly increase the radius further by 516.13 m up to 528.33 m. It can be confirmed, that indeed the dominant value is due to J_2 .

Computational results for longitudinal acceleration $\ddot{\lambda}$ as function of λ are shown in Figure 6. Here it can also be observed, that the largest contribution is due to J_{22} . The values of longitudinal acceleration vary between -0.59007×10^{-3} degrees/day² and 0.65853×10^{-3} degrees/day². For $\lambda = 77.5^\circ$ up to 160° and for $\lambda = 255^\circ$ up to 347.5° , the satellite experiences an acceleration

at the same direction as the rotational speed of the earth, while otherwise it experiences an acceleration in the opposite direction.

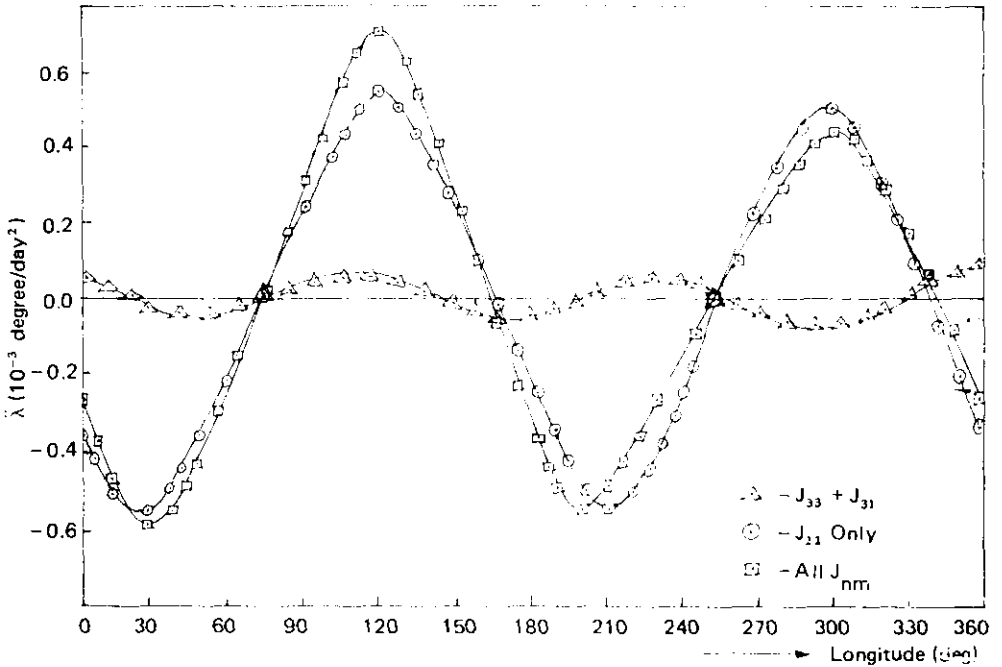


Figure 6 Longitudinal Acceleration

For Keplerian orbit, all points are stationary and located at the equatorial plane on a ring with a radius of $r_0 = 42164.26687$ km. However, the influence of the gravitational anomaly reduces the number of stationary points to four, and they are not precisely located at the equatorial plane. Computational results for stationary points are tabulated in Table 3.

TABLE 3. Equilibrium Positions (GEM 8)

Position	r_0 (km)	λ_0 (deg)	δ_0 (rad)
1	42164.7830	75.0238	-3.5880×10^{-8}
2	42164.7952	162.0093	0.4805×10^{-8}
3	42164.7847	254.7888	-2.7790×10^{-8}
4	42164.7936	348.3743	0.6912×10^{-8}

The trajectories of the satellite about stationary points for various values of inclination i are shown in Figures 7, 8 and 9.

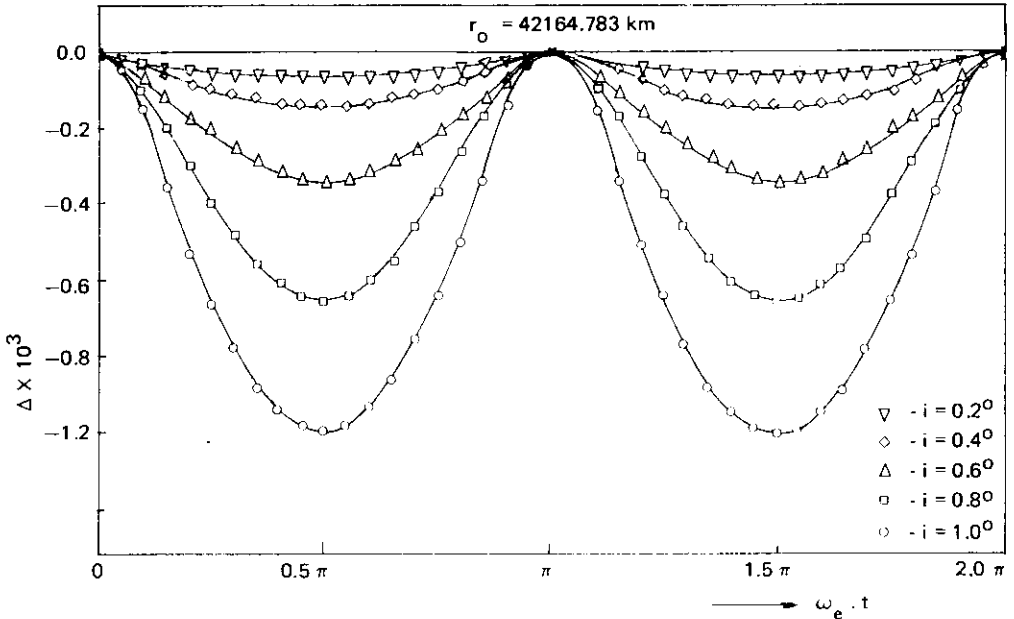


Figure 7 Variation of orbital radius as function of time

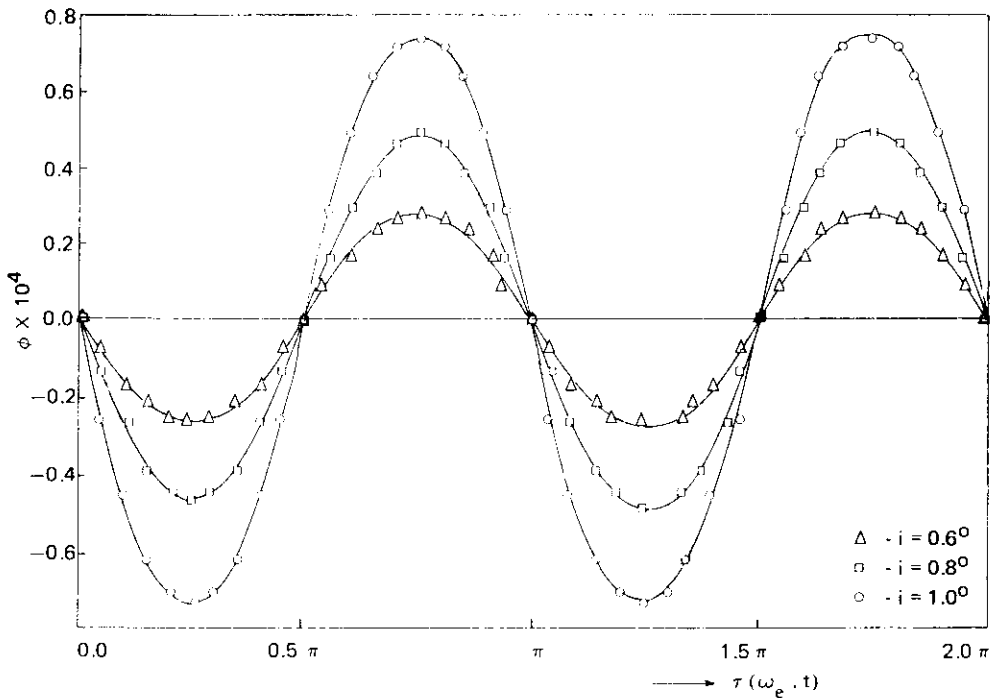


Figure 8 Longitude variation of stationary point as function of time

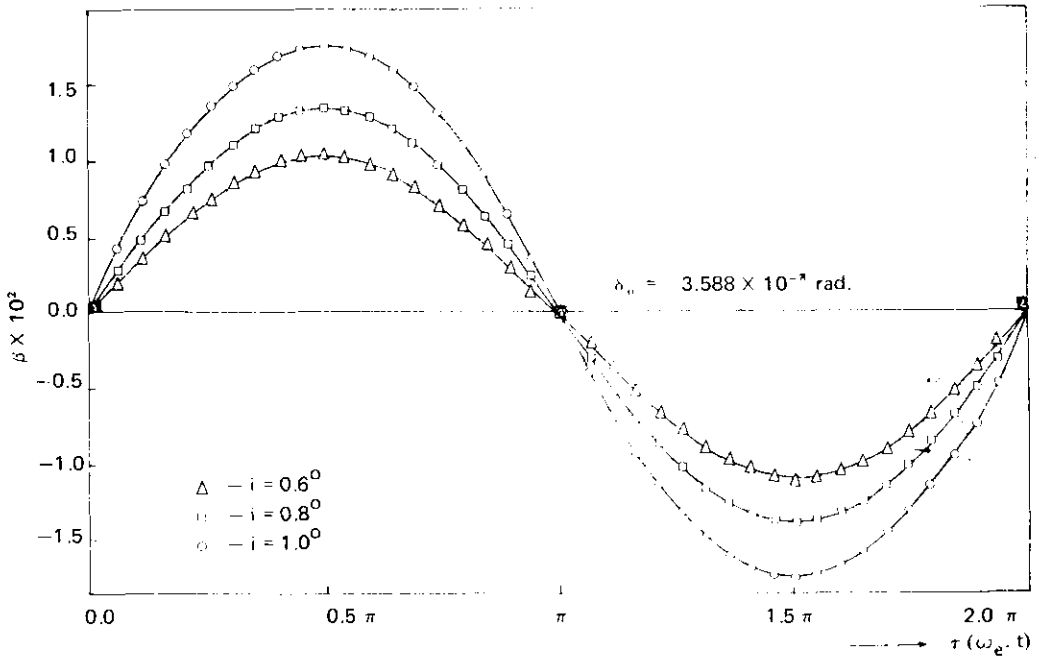


Figure 9 Variation of the latitude of stationary point as function of time

These figures exhibit changes of satellite positions from its stationary points in one cycle (one revolution around the earth), which has a period of one day. The corresponding subsatellite trajectories (or ground tracks) with well known figure 8 configuration for various values of inclination i are shown in Figure 10; for larger inclination, the ground track is also larger.

Assessment of Computational Results

To assess the accuracy and validity of the computational scheme, comparison will be made with results obtained by previous workers. By employing data used by Blitzer⁽⁵⁾, i.e. J_n following King - Hele (1964) and J_{nm} following Izsak (1964)⁽⁵⁾, present results will be compared with Blitzer's⁽⁵⁾. Blitzer utilizes the following formula :

$$z_0 = 6.63$$

$$\lambda_0 = \lambda_{22} + \frac{s\pi}{2} - \frac{\sum_{\substack{(n-m) \\ \text{even}}} \sum \frac{m J_{nm} A_{nm}}{z_0^n} \sin m (\lambda_{22} - \lambda_{nm} + \frac{s\pi}{2})}{\sum_{\substack{(n-m) \\ \text{even}}} \sum \frac{m^2 J_{nm} A_{nm}}{z_0^n} \sin m (\lambda_{22} - \lambda_{nm} + \frac{s\pi}{2})} \quad (32)$$

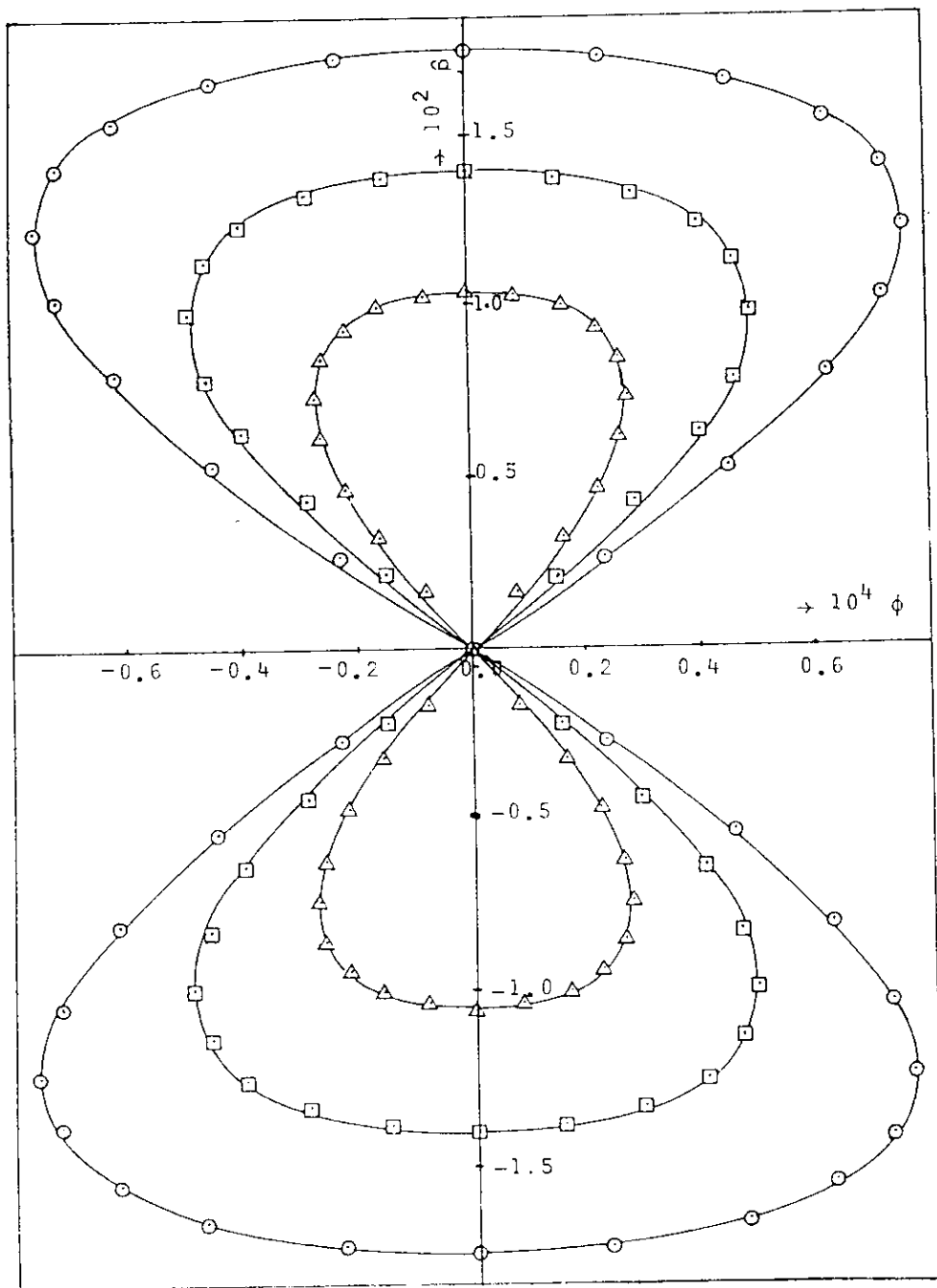


Figure 10 Ground track (subsatellite trajectory) about stationary point for various inclination of orbit.

$$\delta_0 = - \sum_{\substack{n \\ (\text{odd})}} \frac{J_n B_n}{z_0^n} + \sum_{\substack{n, m \\ (\text{odd})}} \frac{J_{nm} B_{nm}}{z_0^n} \cos m (\lambda_0 - \lambda_{nm})$$

where $s = 1, 2, 3, 4$.

Using formula (32), Blitzer arrived at values of stationary positions shown in Table 4. If these values are substituted in equation (25), the right hand side will be equal to $\approx 10^{-9}$, while using similar basic data, we obtain values of stationary positions which are very close to Blitzer's results, as also shown in Table 4. However, if our values are substituted in equation (25), the right hand side will be closer to zero, i.e. 10^{-18} .

TABLE 4. Comparison of Equilibrium Position results with Blitzer's

Position	z_0	Present Method		L. Blitzer's	
		λ_0 (deg)	$10^4 \times \delta_0$ (sec)	λ_0 (deg)	$10^4 \times \delta_0$ (sec)
1	6.63	- 15,201	-10,456	- 15,2	-11
2	6.63	75,052	-37,374	75,1	-37
3	6.63	161,708	-15,823	161,7	-16
4	6.63	-110,861	-43,965	-110,9	-44

The subsatellite trajectory results will be compared to Flury's. According to Flury⁽⁸⁾, the subsatellite trajectory is represented by

$$\delta r = \delta a - \delta a e \cos M = \delta a - \delta a \eta \cos \lambda - \delta a \xi \sin \lambda$$

$$\delta L = 2 e \sin M + (n - \omega_c) t = 2 \eta \sin \lambda - 2 \xi \cos \lambda + (n - \omega_c) t$$

$$\delta \phi = i \sin (\omega + M) = \beta \sin \lambda - \alpha \cos \lambda$$

where :

$$\eta = e \cos (\Omega + \omega), \xi = e \sin (\Omega + \omega)$$

$$\alpha = \sin i \sin \Omega, \beta = \sin i \cos \Omega$$

$M = n t$, $n =$ mean motion

$L =$ longitude

$\lambda = (\Omega + \omega + M)$

As indicated by Table 5, the agreement of our results with Flury's is indeed excellent.

TABLE 5. Comparison of Ground-Track results (GEM 8) with Flury's

inclination (deg)	Present Method		Flury's	
	width (rad)	height (rad)	width (rad)	height (rad)
0,1	$0,761545 \times 10^{-6}$	$0,349060 \times 10^{-2}$	$0,761543 \times 10^{-6}$	$0,349065 \times 10^{-2}$
0,2	$0,304620 \times 10^{-5}$	$0,698100 \times 10^{-2}$	$0,304617 \times 10^{-5}$	$0,698131 \times 10^{-2}$
0,3	$0,685388 \times 10^{-5}$	$0,104716 \times 10^{-1}$	$0,685389 \times 10^{-5}$	$0,104719 \times 10^{-1}$
0,4	$0,121850 \times 10^{-4}$	$0,139620 \times 10^{-1}$	$0,121860 \times 10^{-4}$	$0,139626 \times 10^{-1}$
0,5	$0,190385 \times 10^{-4}$	$0,174524 \times 10^{-1}$	$0,190385 \times 10^{-4}$	$0,174532 \times 10^{-1}$
0,6	$0,274153 \times 10^{-4}$	$0,209420 \times 10^{-1}$	$0,274155 \times 10^{-4}$	$0,209439 \times 10^{-1}$
0,7	$0,373153 \times 10^{-4}$	$0,244340 \times 10^{-1}$	$0,373156 \times 10^{-4}$	$0,244346 \times 10^{-1}$
0,8	$0,487380 \times 10^{-4}$	$0,279240 \times 10^{-1}$	$0,487387 \times 10^{-4}$	$0,279252 \times 10^{-1}$
0,9	$0,616838 \times 10^{-4}$	$0,314140 \times 10^{-1}$	$0,616850 \times 10^{-4}$	$0,314159 \times 10^{-1}$
1,0	$0,761525 \times 10^{-4}$	$0,349040 \times 10^{-1}$	$0,761543 \times 10^{-4}$	$0,349065 \times 10^{-1}$

Comparison of IAU 1968 and GEM 8 results

Satellite coefficients have now been obtained with increasing accuracy; the latest information known to the authors is known as GEM-10, with higher order coefficients in the range of hundredth. However, in the time of writing, only data of GEM-8 and IAU 1968 are available. Preliminary work using IAU 1968 data was reported in reference 9. Comparison of results using these sets of data and present method is intended to investigate further whether the computational accuracy is adequate.

Results are tabulated in Table 6 and 7; it seems that there are some discrepancies, although they are small. However, these results can give confidence in the present computational scheme. It should be noted that computational accuracy is very important, since, due to the fact that satellite follows similar paths repeatedly, resonance may occur, giving rise to larger disturbances originating from smaller ones.

Table 6 Comparison of stellite trajectory (eq. 28, 29 and 30) using GEM-8 and IAU 1968 data, for inclination 0.2°

τ ($\omega_e \cdot t$)	GEM - 8			IAU 1968		
	$\Delta \times 10^4$	$\phi \times 10^5$	$\beta \times 10^2$	$\Delta \times 10^4$	$\phi \times 10^5$	$\beta \times 10^2$
0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
0.15708	-0.00969	-0.09417	0.05461	-0.00890	-0.08903	0.05190
0.31416	-0.03815	-0.17920	0.10787	-0.03662	-0.17516	0.10526
0.47124	-0.08258	-0.24677	0.15847	-0.08047	-0.24360	0.15602
0.62832	-0.13865	-0.29026	0.20517	-0.13615	-0.28820	0.20295
0.78540	-0.20085	-0.30542	0.24682	-0.19822	-0.30459	0.24488
0.94248	-0.26310	-0.29075	0.28240	-0.26100	-0.29116	0.28078
1.09960	-0.31931	-0.24771	0.31101	-0.31718	-0.24923	0.30976
1.25660	-0.36398	-0.18050	0.33197	-0.36242	-0.18291	0.33112
1.41370	-0.39272	-0.09570	0.34476	-0.39190	-0.09868	0.34432
1.57080	-0.40274	-0.00161	0.34905	-0.40273	-0.00480	0.34904
1.72790	-0.39305	0.09256	0.34475	-0.39385	0.08955	0.34517
1.88500	-0.36459	0.17758	0.33196	-0.36613	0.17513	0.33280
2.04200	-0.32015	0.24514	0.31100	-0.32228	0.24357	0.31223
2.19910	-0.26409	0.28862	0.28237	-0.26660	0.28816	0.28398
2.35620	-0.20189	0.30377	0.24680	-0.20453	0.30454	0.24873
2.51330	-0.13963	0.28910	0.20514	-0.14215	0.29110	0.20735
2.67040	-0.08342	0.24605	0.15844	-0.08557	0.24917	0.16087
2.82740	-0.03876	0.17883	0.10783	-0.04033	0.18284	0.11043
2.98450	-0.01001	0.09403	0.05457	-0.01085	0.09860	0.05727
3.14160	-0.00000	-0.00007	-0.00004	-0.00001	0.00472	0.00270
3.29870	-0.00969	-0.09424	-0.05465	-0.00890	-0.08964	-0.05194
3.45580	-0.03815	-0.17927	-0.10791	-0.03662	-0.17523	-0.10529
3.61280	-0.08259	-0.24683	-0.15851	-0.08047	-0.24367	-0.15606
3.76990	-0.13866	-0.29032	-0.20521	-0.13616	-0.28826	-0.20298
3.92700	-0.20086	-0.30547	-0.24685	-0.19823	-0.30464	-0.24491
4.08410	-0.26312	-0.29080	-0.28242	-0.26061	-0.29120	-0.28080
4.24120	-0.31933	-0.24774	-0.31103	-0.31720	-0.24927	-0.30978
4.39820	-0.36400	-0.18052	-0.33199	-0.36244	-0.18294	-0.33113
4.55530	-0.39275	-0.09571	-0.34476	-0.39193	-0.09870	-0.34432
4.71240	-0.40276	-0.00161	-0.34905	-0.40276	-0.00480	-0.34904
4.86950	-0.39307	0.09256	-0.34474	-0.39388	0.08956	-0.34596
5.02650	-0.36461	0.17760	-0.33195	-0.36616	0.17515	-0.33279
5.18360	-0.32018	0.24517	-0.31098	-0.32231	0.24360	-0.31221
5.34070	-0.26411	0.28866	-0.28235	-0.26662	0.28820	-0.28395
5.49780	-0.20191	0.30382	-0.24677	-0.20455	0.30458	-0.24870
5.65490	-0.13965	0.28916	-0.20511	0.14217	0.29116	-0.20732
5.81190	-0.08344	0.24611	-0.15840	-0.08559	0.24923	-0.16084
5.96900	-0.03877	0.17890	-0.10779	-0.04034	0.18290	-0.11039
6.12610	-0.01001	0.09409	-0.05453	-0.01086	0.09867	-0.05723
6.28320	0.00000	0.00000	0.00008	-0.00002	0.00478	-0.00266

Table 7 Comparison of satellite trajectory (eq. 29, 29 and 30) using GEM-8 and IAU 1968 data, for inclination 0.6°

τ ($\omega_e \cdot t$)	GEM - 8			IAU 1968		
	$\Delta \times 10^4$	$\phi \times 10^5$	$\beta \times 10^2$	$\Delta \times 10^4$	$\phi \times 10^5$	$\beta \times 10^2$
0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
0.15708	-0.08724	-0.84753	0.16381	-0.08012	-0.80612	0.15569
0.31416	-0.34334	-1.61280	0.32360	-0.32959	-1.57640	0.35176
0.47124	-0.74325	-2.22090	0.47541	-0.72421	-2.19236	0.46807
0.62832	-1.24780	-2.61230	0.61551	-1.22534	-2.59373	0.60884
0.78540	-1.80760	-2.74870	0.74046	-1.78395	-2.74120	0.73462
0.94248	-2.36790	-2.61680	0.84718	-2.34533	-2.62035	0.84232
1.09960	-2.87380	-2.22940	0.93303	-2.85455	-2.24300	0.92927
1.25660	-3.27580	-1.62440	0.99590	-3.26176	-1.64609	0.99333
1.41370	-3.53460	-0.86122	1.03430	-3.52709	-0.88806	1.03294
1.57080	-3.62470	-0.01440	1.04710	-3.62458	-0.04311	1.04711
1.72790	-3.53750	0.83311	1.03420	-3.54467	0.80606	1.03549
1.88500	-3.28140	1.59840	0.99587	-3.29520	1.57631	0.99838
2.04200	-2.88150	2.20540	0.93297	-2.90058	2.19226	0.93668
2.19910	-2.37690	2.59780	0.84710	-2.39944	2.59360	0.85191
2.35620	-1.81710	2.73420	0.74038	-1.84083	2.74105	0.74617
2.51330	-1.25680	2.60220	0.61541	-1.27944	2.62017	0.62205
2.67040	-0.75089	2.21480	0.47530	-0.77022	2.24280	0.48261
2.82740	-0.34889	1.60990	0.32348	-0.36302	1.64588	0.33129
2.98450	-0.09015	0.84663	0.16369	-0.09769	0.88782	0.17181
3.14160	0.00001	-0.00020	0.00012	-0.00020	0.04285	0.00810
3.29870	-0.08724	-0.84773	-0.16393	-0.08011	-0.80633	-0.15581
3.45580	-0.34335	-1.61300	-0.32371	-0.32959	-1.57660	-0.31588
3.61280	-0.74327	-2.22110	-0.47552	-0.72422	-2.19256	-0.46817
3.76990	-1.24780	-2.61250	-0.61561	-1.22537	-2.59391	-0.60894
3.9270	-1.80770	-2.74890	-0.74055	-1.78398	-2.74136	-0.73471
4.08410	-2.36800	-2.61690	-0.84725	-2.34358	-2.62048	-0.84239
4.24120	-2.87390	-2.22950	-0.93308	-2.85461	-2.24311	-0.92932
4.39820	-3.27590	-1.62450	-0.99594	-3.26182	-1.64617	-0.99337
4.55530	-3.53460	-0.86126	-1.03430	-3.52716	-0.88811	-1.03296
4.71240	-3.62480	-0.01441	-1.04710	-3.62465	-0.04312	-1.04711
4.86950	-3.53750	0.83313	-1.03420	-3.54475	0.80607	-1.03547
5.02650	-3.28140	1.59840	-0.99583	-3.29527	1.57636	-0.99834
5.18360	-2.88150	2.20650	-0.93292	-2.90065	2.19234	-0.93662
5.34070	-2.37700	2.59790	-0.84703	-2.39951	2.59371	-0.85184
5.49780	-1.81710	2.73430	-0.74029	-1.84090	2.74118	-0.74608
5.65490	-1.25680	2.60240	-0.61532	-1.27950	2.62033	-0.62195
5.81190	-0.75093	2.21500	-0.47519	-0.77027	2.24298	-0.48250
5.96900	-0.34892	1.61010	-0.32336	-0.36306	1.64606	-0.33118
6.12610	-0.09017	0.84633	-0.16357	-0.09772	0.88802	-0.17169
6.28320	-0.00000	0.00000	-0.00024	-0.00022	0.04053	-0.00798

VIII. CONCLUDING REMARKS

A computational scheme to calculate the orbit of geostationary satellite due to the earth's gravitational potential has been developed, taking special care to the influence of the gravitational anomaly. Results obtained have been compared to those of Blitzer and Flury, and established confidence in the present scheme. Further development is planned to account for the effect of the moon, the sun and solar radiation pressure.

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